

**COMP.SGN.100 Introduction to Signal Processing,
Final Exam, 20.10.2021,
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- Own calculators can be used in the exam.
- You may take the examination paper with you.

1. Below are three systems S1-S3

$$S1: y(n) = \sqrt{x(n)},$$

$$S2: y(n) = x(n) + x(n-1) + 2x(n+1),$$

$$S3: y(n) = x(n) + 3x(n+2).$$

Which of these systems are

- (a) causal,
- (b) memoryless,
- (c) linear.

Justify your answers. (6p)

2. (a) Calculate the DFT of the vector $x(n) = (4, 6, 3, 3)^T$. (3p)
- (b) The signal $x(n)$ and the impulse response $h(n)$ are the following:

$$x(n) = \delta(n) + \delta(n-1) - 2\delta(n-2),$$

$$h(n) = \delta(n+2) - \delta(n).$$

Draw the signals $x(n)$ and $h(n)$. Calculate the signal $y(n) = h(n) * x(n)$ and draw it. (3p)

3. The signal $x(n)$ with the sampling rate 40 kHz should be converted to a signal with the sampling rate 25 kHz. Determine the steps of the conversion as a block diagram using re-sampling ($\uparrow L$ and $\downarrow M$) and low-pass filtering ($H(z)$). Specify the passband, stopband and transition band intervals of the required low-pass filters in normalized frequencies, when the frequencies on the interval 0 – 12 kHz are to be preserved. (6p)
4. Design using the window design method a filter (i.e. find out its impulse response) satisfying the following requirements:

Stopband	[0 kHz, 17 kHz]
Passband	[19 kHz, 25 kHz]
Passband ripple	0.5 dB
Minimum stopband attenuation	28 dB
Sampling frequency	50 kHz

Use the tables below. (6p)

5. (a) The transfer function of a causal LTI system is:

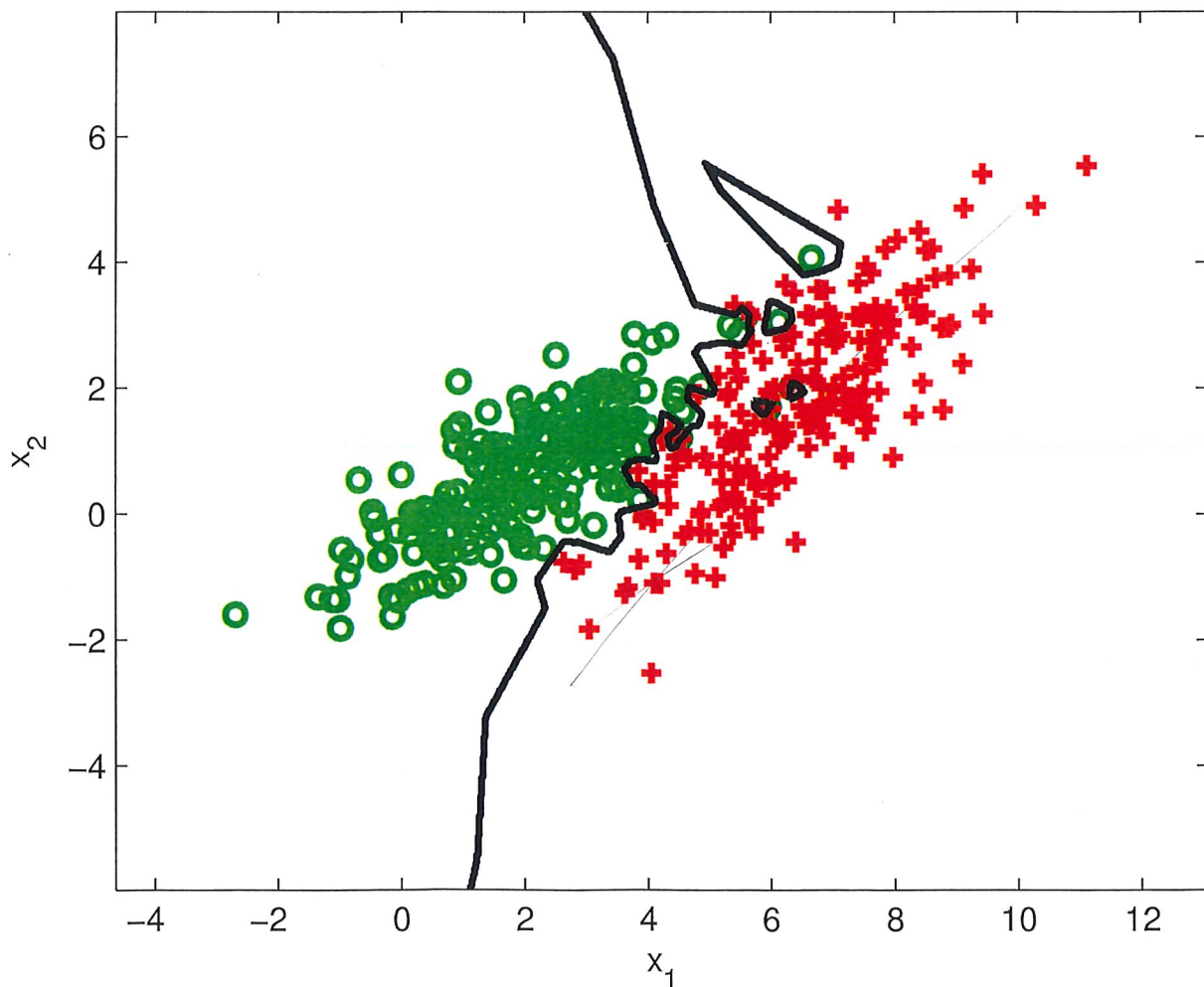
$$H(z) = \frac{1 - az^{-1}}{1 - \frac{1}{2}(bz)^{-1}},$$

where the nonzero constants $a, b \in \mathbb{R}$. Determine which values of the constants a and b make the system stable. (3p)

- (b) Below is shown the decision boundary obtained using a classifier for a two-class classification task. Is it possible that the used classifier was

- i. 1-NN classifier,
- ii. 9-NN classifier,
- iii. LDA classifier?

Justify your answers. (3p)



Tables

Ideal filter type	Impulse response when	
	$n \neq 0$	$n = 0$
Low-pass	$2f_c \text{sinc}(n \cdot 2\pi f_c)$	$2f_c$
High-pass	$-2f_c \text{sinc}(n \cdot 2\pi f_c)$	$1 - 2f_c$
Band-pass	$2f_2 \text{sinc}(n \cdot 2\pi f_2) - 2f_1 \text{sinc}(n \cdot 2\pi f_1)$	$2(f_2 - f_1)$
Band-stop	$2f_1 \text{sinc}(n \cdot 2\pi f_1) - 2f_2 \text{sinc}(n \cdot 2\pi f_2)$	$1 - 2(f_2 - f_1)$

Name of the window function	Transition bandwidth (normalized)	Passband ripple (dB)	Minimum stopband attenuation (dB)	Window expression $w(n)$, when $ n \leq (N-1)/2$
Rectangular	$0.9/N$	0.7416	21	1
Bartlett	$3.05/N$	0.4752	25	$1 - \frac{2 n }{N-1}$
Hanning	$3.1/N$	0.0546	44	$0.5 + 0.5 \cos\left(\frac{2\pi n}{N}\right)$
Hamming	$3.3/N$	0.0194	53	$0.54 + 0.46 \cos\left(\frac{2\pi n}{N}\right)$
Blackman	$5.5/N$	0.0017	74	$0.42 + 0.5 \cos\left(\frac{2\pi n}{N}\right) + 0.08 \cos\left(\frac{4\pi n}{N}\right)$

Some Wikipedia pages that might be useful

Suppose two classes of observations have means $\vec{\mu}_0, \vec{\mu}_1$ and covariances Σ_0, Σ_1 . Then the linear combination of features $\vec{w} \cdot \vec{x}$ will have means $\vec{w} \cdot \vec{\mu}_i$ and variances $\vec{w}^T \Sigma_i \vec{w}$ for $i = 0, 1$. Fisher defined the separation between these two distributions to be the ratio of the variance between the classes to the variance within the classes:

$$S = \frac{\sigma_{\text{between}}^2}{\sigma_{\text{within}}^2} = \frac{(\vec{w} \cdot \vec{\mu}_1 - \vec{w} \cdot \vec{\mu}_0)^2}{\vec{w}^T \Sigma_1 \vec{w} + \vec{w}^T \Sigma_0 \vec{w}} = \frac{(\vec{w} \cdot (\vec{\mu}_1 - \vec{\mu}_0))^2}{\vec{w}^T (\Sigma_0 + \Sigma_1) \vec{w}}$$

This measure is, in some sense, a measure of the signal-to-noise ratio for the class labelling. It can be shown that the maximum separation occurs when

$$\vec{w} \propto (\Sigma_0 + \Sigma_1)^{-1} (\vec{\mu}_1 - \vec{\mu}_0)$$

When the assumptions of LDA are satisfied, the above equation is equivalent to LDA.

Be sure to note that the vector \vec{w} is the normal to the discriminant hyperplane. As an example, in a two dimensional problem, the line that best divides the two groups is perpendicular to \vec{w} .

Generally, the data points to be discriminated are projected onto \vec{w} ; then the threshold that best separates the data is chosen from analysis of the one-dimensional distribution. There is no general rule for the threshold. However, if projections of points from both classes exhibit approximately the same distributions, a good choice would be the hyperplane between projections of the two means, $\vec{w} \cdot \vec{\mu}_0$ and $\vec{w} \cdot \vec{\mu}_1$. In this case the parameter c in threshold condition $\vec{w} \cdot \vec{x} > c$ can be found explicitly:

$$c = \vec{w} \cdot \frac{1}{2} (\vec{\mu}_0 + \vec{\mu}_1) = \frac{1}{2} \vec{\mu}_1^T \Sigma_1^{-1} \vec{\mu}_1 - \frac{1}{2} \vec{\mu}_0^T \Sigma_0^{-1} \vec{\mu}_0.$$

Inversion of 2×2 matrices [edit]

The cofactor equation listed above yields the following result for 2×2 matrices. Inversion of these matrices can be done as follows:^[6]

$$\mathbf{A}^{-1} = \begin{bmatrix} a & b \\ c & d \end{bmatrix}^{-1} = \frac{1}{\det \mathbf{A}} \begin{bmatrix} d & -b \\ -c & a \end{bmatrix} = \frac{1}{ad - bc} \begin{bmatrix} d & -b \\ -c & a \end{bmatrix}.$$

A more condensed form of the difference equation is:

$$y[n] = \frac{1}{a_0} \left(\sum_{i=0}^P b_i x[n-i] - \sum_{j=1}^Q a_j y[n-j] \right)$$

which, when rearranged, becomes:

$$\sum_{j=0}^Q a_j y[n-j] = \sum_{i=0}^P b_i x[n-i]$$

To find the **transfer function** of the filter, we first take the **Z-transform** of each side of the above equation, where we use the **time-shift property** to obtain:

$$\sum_{j=0}^Q a_j z^{-j} Y(z) = \sum_{i=0}^P b_i z^{-i} X(z)$$

We define the **transfer function** to be:

$$\begin{aligned} H(z) &= \frac{Y(z)}{X(z)} \\ &= \frac{\sum_{i=0}^P b_i z^{-i}}{\sum_{j=0}^Q a_j z^{-j}} \end{aligned}$$

Considering that in most IIR filter designs coefficient a_0 is 1, the IIR filter transfer function takes the more traditional form:

$$H(z) = \frac{\sum_{i=0}^P b_i z^{-i}}{1 + \sum_{j=1}^Q a_j z^{-j}}$$

Techniques [\[edit \]](#)

Conceptual approaches to sample-rate conversion include: converting to an analog continuous signal, then re-sampling at the new rate, or **calculating** the values of the new samples directly from the old samples. The latter approach is more satisfactory, since it introduces less noise and distortion.^[3] Two possible implementation methods are as follows:

1. If the ratio of the two sample rates is (or can be approximated by)^{[nb 1][4]} a fixed rational number L/M : generate an intermediate signal by inserting $L - 1$ 0s between each of the original samples. Low-pass filter this signal at half of the lower of the two rates. Select every M -th sample from the filtered output, to obtain the result.^[5]
2. Treat the samples as geometric points and create any needed new points by interpolation. Choosing an interpolation method is a trade-off between implementation complexity and conversion quality (according to application requirements). Commonly used are: **ZOH** (for film/video frames), **cubic** (for image processing) and **windowed sinc function** (for audio).

Equations

$$ax^2 + bx + c = 0 \Leftrightarrow x = \frac{-b \pm \sqrt{b^2 - 4ac}}{2a}$$

$$\begin{cases} X(n) = X_0(n) + w_N^{-n} X_1(n), & \text{when } n = 0, 1, 2, \dots, N/2 - 1 \\ X(n) = X_0(n - N/2) + w_N^{-n} X_1(n - N/2), & \text{when } n = N/2, N/2 + 1, \dots, N - 1 \end{cases}$$